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AREA FRACTION FRACTIONATOR

Estimated volume fraction (\widehat{V}_{ν})	$\widehat{V_{v}}(Y, ref) = \frac{\sum_{i=1}^{m} P(Y)_{i}}{\sum_{i=1}^{m} P(ref)_{i}}$	 P(ref) Points hitting reference volume Y Sub-region P(Y) Points hitting sub-region
Estimated area (\hat{A})	$\hat{A} = \frac{1}{asf} \cdot a(p) \cdot P(Y_i)$	asf Area sampling fraction $a(p)$ Area associated with a point

References

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CAVALIERI ESTIMATOR

Area associated with a point (A_p)	$A_p = g^2$	g^2 Grid area
Volume associated with a point (V _P)	$V_p = g^2 m \bar{t}$	m Section evaluation interval \bar{t} Mean section cut thickness
Estimated volume (ν)	$\widehat{V} = A_p m' \overline{t} \left(\sum_{i=1}^n P_i \right)$	A_p Area associated with a point m' Section evaluation interval \overline{t} Mean section cut thickness P_i Points counted on grid
Estimated volume corrected for over-projection ([v])	$[v] = t \cdot \left(k \cdot \sum_{j=1}^{g} a'_j - max(a')\right)$	<i>t</i> Section cut thickness <i>k</i> Correction factor <i>g</i> Grid size <i>a</i> ' Projected area
Coefficient of error (CE)	$CE = \frac{\sqrt{TotalVar}}{\sum_{i=1}^{n} P_i}$	TotalVar Total variance of the estimated volume n Number of sections P_i Points counted on gridTotalVar = $s^2 + VAR_{SRS}$



Cavalieri Estimator (2)

Variance of systematic random sampling (VAR _{SRS})	$VAR_{SRS} = \frac{3(A - s^2) - 4B + C}{12}, m = 0$ $VAR_{SRS} = \frac{3(A - s^2) - 4B + C}{240}, m = 1$	<i>m</i> Smoothness class of sampled function s^2 Variance due to noise $A = \sum_{i=1}^{n} P_i^2$, $B = \sum_{i=1}^{n-1} P_i P_{i+1}$, $C = \sum_{i=1}^{n-2} P_i P_{i+2}$ With: <i>n</i> : number of sections $s^2 = 0.0724 \left(\frac{b}{2}\right) \sqrt{n \sum_{i=1}^{n} P_i}$
		$\frac{b}{\sqrt{a}}$ Shape factor

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CYCLOIDS FOR LV

Area associated with a point (A_p)	$A_p = g^2$	g^2 Grid area
Volume associated with a point (V_p)	$V_p = g^2 m \bar{t}$	g^2 Grid area <i>m</i> Section evaluation interval \overline{t} Mean section cut thickness
Length per unit volume (L_{ν})	$L_{V} = 2 \frac{\left[\bar{I}_{L}^{C}\right]_{prj}}{\Delta}$ $L_{V} = \frac{2}{\Delta} \cdot \frac{\left(\bar{I}_{c}^{cyc}\right)_{prj}}{\bar{P} \cdot \left(\frac{l}{p}\right)} = \frac{2}{\Delta} \left(\frac{p}{p}\right) \frac{\sum_{i=1}^{n} I_{i}}{\sum_{i=1}^{n} P_{i}}$	$\left[\overline{I}_{L}^{C}\right]_{prj}$ Number of counting frames Δ Section cut thickness I_{i} Intercepts P_{i} Test points $\left[\overline{I}_{C}^{cyc}\right]_{prj}$ Average number of intersections of projected images $\frac{p}{1}$ Test points per unit length of cycloid
Estimated volume (疗)	$\hat{V} = m\Delta\left(\frac{a}{p}\right)\sum_{i=1}^{n} P_i$	m Sampling fractions Δ Section cut thickness a Area p Number of test points P_i Test points
Estimated length (\hat{L})	$\hat{L} = 2\left(\frac{a}{l}\right)m\sum_{i=1}^{n}I_{i}$	<i>a</i> Area <i>I</i> Line length <i>m</i> Sampling fractions <i>Ii</i> Intercepts



Cycloids for Lv (2)

Coefficient of error for line length	$CE(\hat{L} L) = \frac{\sqrt{VAR_{SRS}}}{\sum_{i=1}^{n} I_i}$	VAR_{SRS} Variance of systematic random sampling $\widehat{L} L$ Estimated length per length I_i Intercepts
Variance of systematic random sampling (VAR _{SRS})	$VAR_{SRS} = \frac{3g_0 - 4g_1 + g_2}{12}$	g Grid size L_i Line length at section i
	$g_k = \sum_{i=1}^{n-k} L_i L_{i+k}$	

Coefficient of error for length density	$CE(L_V) = \sqrt{\frac{n}{n-1} \left(\frac{\sum_{i=1}^{n} I_i^2}{\sum_{i=1}^{n} I_i \sum_{i=1}^{n} I_i} + \frac{\sum_{i=1}^{n} P_i^2}{\sum_{i=1}^{n} P_i \sum_{i=1}^{n} P_i} - 2 \frac{\sum_{i=1}^{n} I_i P_i}{\sum_{i=1}^{n} I_i \sum_{i=1}^{n} P_i} \right)}$	<i>Ii</i> Intercepts <i>Pi</i> Test points <i>n</i> Number of probes
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IMAGE VOLUME FRACTIONATOR

Estimate of total number of particles (<i>N</i>)	$N = \sum Q^- \cdot \frac{1}{asf} \cdot \frac{1}{zsf}$	Q^- Particles counted asf Area sampling fraction (counting frame/grid size) zsf Section sampling fraction (disector height/virtual section thickness)
Variance due to systematic random sampling – Gundersen (VARsRs)	$VAR_{SRS} = \frac{3(A - s^2) - 4B + C}{12}, m$ $= 0$ $VAR_{SRS} = \frac{3(A - s^2) - 4B + C}{240}, m$ $= 1$	$A = \sum_{i=1}^{n} (Q_i^{-})^2$ $B = \sum_{i=1}^{n-1} Q_i^{-} Q_{i+1}^{-}$ $C = \sum_{i=1}^{n-2} Q_i^{-} Q_{i+2}^{-}$ $s^2 \text{ Variance due to noise}$
Variance due to noise - Gundersen (S ²)	$s^2 = \sum_{i=1}^n Q^-$	Q^- Particles counted n Number of sections used
Total variance – Gundersen (<i>TotalVar</i>)	$TotalVar = s^2 + VAR_{SRS}$	<i>VAR_{SRS}</i> Variance due to SRS <i>s</i> ² Variance due to noise
Coefficient of error – Gundersen (<i>CE</i>)	$CE = \frac{\sqrt{TotalVar}}{s^2}$	TotalVarTotal variance s^2 Variance due to noise



Image Volume Fractionator (2)

Coefficient of error – Scheaffer (CE)	$CE = \frac{\sqrt{s^2 \left(\frac{1}{f} - \frac{1}{F}\right)}}{\bar{Q}}$	f Number of counting frames F Total possible sampling sites s^2 Estimated variance \overline{Q} Average particles counted
Average number of particles – Scheaffer (\overline{Q})	$\bar{Q} = \frac{\sum_{i=1}^{f} Q_i}{f}$	Q_i Particles counted f Number of counting frames
Estimated variance - Scheaffer (S ²)	$s^{2} = \frac{\sum_{i=1}^{f} (Q_{i} - \bar{Q})^{2}}{f - 1}$	f Number of counting frames Q_i Particles counted $\overline{\mathbf{Q}}$ Average particles counted
Estimated variance of estimated cell population - Scheaffer	$\frac{C_{fp}F^2s^2}{f}$	C_{fp} Finite population correction s^2 Estimated variance f Number of counting frames F Total possible sampling sites
Estimated variance of mean cell count - Scheaffer	$\frac{C_{fp}s^2}{f}$	C_{fp} Finite population correction s^2 Estimated variance f Number of counting frames



Image Volume Fractionator (3)

Estimated mean coefficient of error – Cruz-Orive (<i>est Mean CE</i>)	est Mean CE (est N) = $\left[\frac{1}{3n} \cdot \sum_{i=1}^{n} \left(\frac{Q_{1i} - Q_{2i}}{Q_{1i} + Q_{2i}}\right)^2\right]^{1/2}$	Q_{1i} Counts in sub-sample 1 Q_{2i} Counts in sub-sample 2 n Size of sub-sample
Predicted coefficient of error for estimated population – Schmitz- Hof (<i>CE</i> pred)	$CE_{pred}(n_F) = \sqrt{\frac{Var(Q_r^-)}{R.(Q_r^-)^2}}$ $CE_{pred}(n_F) = \frac{1}{\sqrt{\sum_{r=1}^R Q_r^-}} = \frac{1}{\sqrt{\sum_{s=1}^S Q_s^-}}$	R Number of counting spaces S Number of sections Q_r^- Counts in the "r"-th counting space Q_s^- Counts in the "s"-th section

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Image Volume Fractionator (4)

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Schmitz, C., Hof, P.R. (2000). <u>Recommendations for straightforward and rigorous methods of counting neurons based on a computer simulation approach.</u> Journal of Chemical Neuroanatomy, 20 (1), 93–114.

West, M. J., Slomianka, L., & Gundersen, H.J.G. (1991). <u>Unbiased stereological estimation of the total number of neurons in the</u> subdivisions of the rat hippocampus using the optical fractionator. The Anatomical Record, 231 (4), 482–497.



IMAGE VOLUME SPACEBALLS

Length estimate	$L = 2.\left(\sum_{i=1}^{n} Q_i\right) \cdot \frac{v}{a}$ This equation does not include the terms F2 (area- fraction) and F3 (thickness-fraction) used by Mouton et al. (equation 2, 2002), but includes that information in v (volume sampled).	n Number of sections used Q _i Intersection counted v Volume (grid X * grid Y* section thickness) a Surface area of the sphere
Variance due to noise	$s^2 = \sum_{i=1}^n Q_i$	<i>Q_i</i> Intersection counted
Variance due to systematic random sampling	$VAR_{SRS} = \frac{3(A - s^2) - 4B + C}{12}, m = 0$ $VAR_{SRS} = \frac{3(A - s^2) - 4B + C}{240}, m = 1$	$A = \sum_{i=1}^{n} (Q_i^{-})^2$ $B = \sum_{i=1}^{n-1} Q_i^{-} Q_{i+1}^{-}$ $C = \sum_{i=1}^{n-2} Q_i^{-} Q_{i+2}^{-}$ $s^2 \text{ Variance due to noise}$ m Smoothness class of sampled function
Total variance	$TotalVar = s^2 + VAR_{SRS}$	<i>VAR_{SRS}</i> Variance due to SRS <i>s²</i> Variance due to noise



Image Volume Spaceballs (2)

Coefficient of error	$CE = \frac{\sqrt{TotalVar}}{s^2}$	<i>TotalVar</i> Total variance <i>s</i> ² Variance due to noise
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References

Mouton, P. R., Gokhale, A.M., Ward, N.L., & West, M.J. (2002). <u>Stereological length estimation using spherical probes</u>. *Journal of Microscopy*, *206* (1), 54–64.



ISOTROPIC FAKIR

Estimated total surface area $estS = 2\frac{1}{n} \cdot \sum_{i=1}^{n} \frac{v}{l_i} \cdot I_i$	<i>n</i> Number of line sets (always set to 3) $\frac{v}{l_i}$ Inverse of the probe per unit volume I_i Intercepts with test lines
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NUCLEATOR

Area estimate	$a = \pi \overline{l^2}$	<i>l</i> Length of rays
Volume estimate	$\overline{v_N} = \frac{4\pi}{3} \overline{l_n^3}$	<i>l</i> Length of rays
Estimated coefficient of error	$est \ CV(R) = \frac{\sqrt{\frac{1}{n-1}\sum_{i=1}^{n}(R_i - \bar{R})^2}}{\bar{R}}$	<i>n</i> Number of nucleator estimates R_i Area/volume estimate for each sampling site
Average area/volume estimate	$\bar{R} = \frac{1}{n} \sum_{i=1}^{n} R_i$	n Number of nucleator estimates R_i Area/volume estimate for each sampling site
Relative efficiency	$CE_n(R) = \frac{CV(R)}{\sqrt{n}}$	<i>n</i> Number of nucleator estimates <i>CV (R)</i> Estimated coefficient of variation
Geometric mean of area/volume estimate	$e^{\left(\frac{1}{n}\sum_{i=1}^{n}lnR_{i}\right)}$	<i>n</i> Number of nucleator estimates R_i Area/volume estimate for each sampling site

References

Gundersen, H.J.G. (1988). The nucleator. Journal of Microscopy, 151 (1), 3–21.



OPTICAL ROTATOR

Volume of particle	$\hat{v} = a \sum_{i}^{+/-} g(P_i)$	<i>a</i> Reciprocal line density <i>a=k.h</i> <i>k</i> Length of slice <i>h</i> Systematic spacing
For vertical slabs and lines parallel to vertical axis	$g(P) = d_1, if \ d_2 < t$ $g(P) = \frac{\frac{\pi}{2}d_1}{\arcsin\left(\frac{t}{d_2}\right)}, if \ t \le d_2$	d_1 Distance along test line d_2 Distance from origin to test line t $\frac{1}{2}$ thickness of optical slice
For vertical slabs and lines perpendicular to vertical axis	$g(P) = d_1, if \sqrt{d_1^2 + z^2} < t$ $g(P) = f\left(\sqrt{t^2 - z^2}\right), if z < t \le \sqrt{d_1^2 + z^2}$ $g(P) = f(0), if t \le z $ $f(x) = x + \frac{\pi}{2} \int_x^{d_1} \frac{1}{\arcsin\left(\frac{t}{\sqrt{u^2 + z^2}}\right)} du$	<i>d</i> ¹ Distance along test line <i>t</i> 1/2 thickness of optical slice <i>z</i> Distance in <i>z</i> from intercept to origin



Optical Rotator (2)

For isotropic slabs	$g(P) = d_1, if \ d_3 < t$ $g(P) = \frac{1}{2t} [h(t, d_2) + k(t, d_1, d_2, d_3)], if \ d_2 < t$ $\leq d_3$ $h(t, d) = t^2 \sqrt{1 - \frac{d^2}{t^2}}$ $k(t, d_1, d_2, d_3) = d_1 d_3 + d_2^2 log \left(\frac{d_1 + d_3}{t + \sqrt{t^2 - d_2^2}}\right)$	d_1 Distance along test line d_2 Distance from origin to test line d_3 Distance from intercept to origin t $\frac{1}{2}$ thickness of optical slice
Estimated surface area	$\hat{S} = a \sum_{j} l_{j}g(l_{j})$ $g(l) = 2, if \ d_{2} < t$ $g(l) = \pi \cdot \frac{1}{\arcsin\left(\frac{t}{d_{2}}\right)}, if \ t \le d_{2}$	a Reciprocal line density l_j Number of intersections between grid line and cell boundary d_2 Distance from origin to test line $t \frac{1}{2}$ thickness of optical slice

References

Tandrup, T., Gundersen, H.J.G., & Vedel Jensen, E.B. (1997). The optical rotator Journal of microscopy, 186 (2), 108–120.



PLANAR ROTATOR

Volume for isotropic planar rotator	$V = 2t \sum_{i} g_{i}$	t Separation between test lines g_i Isotropic planar rotator function
Volume for vertical planar rotator	$V = \pi t \sum_{i} l_i^2$	t Separation between test lines l_i Intercept length along a test line
Isotropic planar rotator function	$g_{i}(l) = l\sqrt{l^{2} + a_{i}^{2}} + a_{i}^{2}ln\left[\frac{l}{a_{i}} + \sqrt{\left(\frac{l}{a_{i}}\right)^{2} + 1}\right]$ $g_{i+} = \sum_{j even} g_{i}(l_{i j+}) - \sum_{j odd} g_{i}(l_{i j+})$ $g_{i-} = \sum_{j even} g_{i}(l_{i j-}) - \sum_{j odd} g_{i}(l_{i j-})$ $g_{i} = \frac{1}{2}(g_{i+} + g_{i-})$	 <i>l</i> Intercept length along a test line <i>a</i>_i Distance from origin to test line <i>j</i> Number of grid lines <i>l</i>_{ij} Number of intersections between the j-th grid line and the cell boundary



Planar Rotator (2)

lsotropic planar rotator function (cont'd)	$l_{i+}^{2} = \sum_{j \text{ even}} l_{i j+}^{2} - \sum_{j \text{ odd}} l_{i j+}^{2}$ $l_{i-}^{2} = \sum_{j \text{ even}} l_{i j-}^{2} - \sum_{j \text{ odd}} l_{i j-}^{2}$ $l_{i}^{2} = \frac{1}{2} (l_{i+}^{2} + l_{i-}^{2})$	 <i>l</i> Intercept length along a test line <i>a_i</i> Distance from origin to test line <i>j</i> Number of grid lines <i>l_{ij}</i> Number of intersections between the j-th grid line and the cell boundary

References

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SURFACTOR

Surface area for single-ray designs	$\hat{S} = 4\pi l_0^2 + c(\beta)$	 <i>l</i> Length of intercept <i>fs</i> Angle between test line and surface <i>c(fs)</i> Function of the planar angle
Surface area for multi-ray designs	$\widehat{S} = 2\pi \sum_{j=1}^{2r} l_j^2 \cdot c(\beta)$	 <i>l</i> Length of intercept <i>f</i> Angle between test line and surface <i>c(f</i>) Function of the planar angle <i>r</i> Number of test lines
Function of the planar angle	$c(\beta) = 1 + \left[\frac{1}{2}\cot\beta\right] \cdot \left[\frac{\pi}{2} - \sin^{-1}\frac{1 - \cot^2\beta}{1 + \cot^2\beta}\right]$	ß Angle between test line and surface

References

Jensen, E.B., Gundersen, H.J.G. (1987). Stereological estimation of surface area of arbitrary particles. Acta Stereologica, 6 (3).